TWO-PORT NFTWORKS Linear network

In many situations one is not interested in the internal organization of a network. A description relating input and output variables may be sufficient

A two-port model is a description of a network that relates voltages and currents

at two pairs of torminals

LEARNING

GOALS

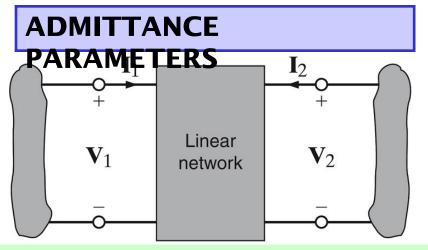
Study the basic types of two-port

models Admittance parameters Impedance parameters Hybrid parameters

Transmission

naramotore

Understand how to convert one model into another



The network contains NO independent

The admittance parameters describe the currents in terms of the

 y_{21} determines the current $I_1 = y_{11}V_1 + y_{12}V_2$ flowing into port 2 when the $I_2 = y_{21}V_1 + y_{22}V_2$ port is short -circuited and a voltage is applied to port 1

$$I_1 = y_{11}V_1 + y_{12}V_2$$

 $I_2 = y_{21}V_1 + y_{22}V_2$

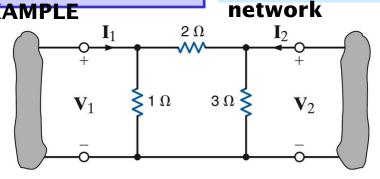
The first subindex identifies the output port. The second the input port.

The computation of the parameters follows directly from the definition

$$y_{11} = \frac{I_1}{V_1}\Big|_{V_2=0}$$
 $y_{12} = \frac{I_1}{V_2}\Big|_{V_1=0}$

$$|y_{21} = \frac{I_2}{V_1}\Big|_{V_2=0}$$
 $|y_{22} = \frac{I_2}{V_2}\Big|_{V_1=0}$

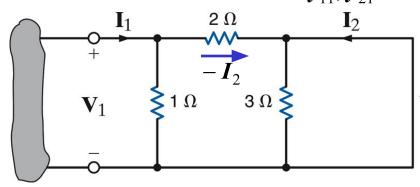
Find the admittance parameters for the



$$I_1 = y_{11}V_1 + y_{12}V_2$$

 $I_2 = y_{21}V_1 + y_{22}V_2$

Circuit used to determine y_{11}, y_{21}



$$I_1 = (1 + \frac{1}{2})V_1 \Rightarrow y_{11} = \frac{3}{2}[S]$$

$$\mathbf{V}_2 = 0 \quad -I_2 = \frac{1}{1+2}I_1 \Rightarrow I_2 = -\frac{1}{2}V_1 \Rightarrow y_{21} = -\frac{1}{2}[S]$$

Circuit used to determine y_{12}, y_{22} $I_1 \qquad 2\Omega \qquad I_2$ $V_1 = 0 \qquad \qquad 1\Omega \qquad 3\Omega \qquad \qquad V_2$

$$I_2 = \left(\frac{1}{2} + \frac{1}{3}\right) V_2 \Rightarrow \mathbf{y}_{22} = \frac{5}{6} [\mathbf{S}]$$

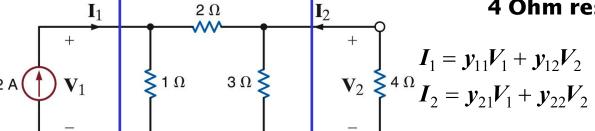
$$-I_1 = \frac{3}{2+3} I_2 = \frac{3 \times 5}{5 \times 6} V_2 \Rightarrow \mathbf{y}_{12} = \frac{1}{2} [\mathbf{S}]$$

Next we show one use of this model

An application of the admittance

Determine the current through the





4 Ohm resistor

$$I_1 = \frac{3}{2}V_1 - \frac{1}{2}V_2$$

$$I_2 = -\frac{1}{2}V_1 + \frac{5}{6}V_2$$

 $I_1 = 2A$, $V_2 = -4I_2$ $I_2 = -\frac{1}{4}V_2$

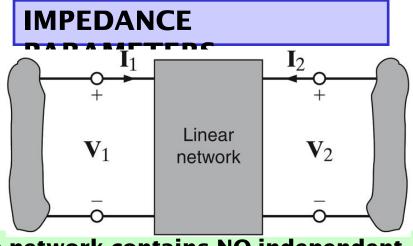
The model plus the conditions at the ports are sufficient to determine the other $y_{\underline{a}}$ riables V_2

$$V_1 = \frac{13}{6}V_2$$

$$V_2 = \frac{8}{11}[V]$$

$$I_2 = -\frac{2}{11}[A]$$

$$0 = -\frac{1}{2}V_1 + \left(\frac{5}{6} + \frac{1}{4}\right)V_2$$



The network contains NO independent sources

$$V_1 = z_{11}I_1 + z_{12}I_2$$

$$V_2 = z_{21}I_1 + z_{22}I_2$$

The 'z parameters' can be derived in a manner similar to the Y parameters

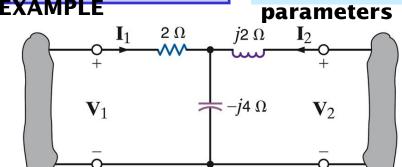
$$\left. \boldsymbol{z}_{11} = \frac{\boldsymbol{V}_1}{\boldsymbol{I}_1} \right|_{\boldsymbol{I}_2 = 0}$$

$$\left. \boldsymbol{z}_{11} = \frac{\boldsymbol{V}_1}{\boldsymbol{I}_1} \right|_{\boldsymbol{I}_2 = 0} \qquad \left. \boldsymbol{z}_{21} = \frac{\boldsymbol{V}_2}{\boldsymbol{I}_1} \right|_{\boldsymbol{I}_2 = 0}$$

$$z_{12} = \frac{V_1}{I_2}\Big|_{I_1=0}$$
 $z_{22} = \frac{V_2}{I_2}\Big|_{I_1=0}$

$$\left. \boldsymbol{z}_{22} = \frac{\boldsymbol{V}_2}{\boldsymbol{I}_2} \right|_{\boldsymbol{I}_1 = 0}$$

Find the Z parameters



$$V_1 = z_{11}I_1 + z_{12}I_2$$

$$V_2 = z_{21}I_1 + z_{22}I_2$$

$$z_{11} = \frac{V_1}{I_1}\Big|_{I_2=0}$$
 $z_{21} = \frac{V_2}{I_1}\Big|_{I_2=0}$

$$\tilde{V}_1 = 2I_1 - j4(I_1 + I_2)$$

$$V_2 = j2I_2 - j4(I_2 + I_1)$$

$$z_{12} = \frac{V_1}{I_2}\Big|_{I_1=0}$$
 $z_{22} = \frac{V_2}{I_2}\Big|_{I_1=0}$

$$\boldsymbol{z}_{22} = \frac{\boldsymbol{V}_2}{\boldsymbol{I}_2}\bigg|_{\boldsymbol{I}_1 = 0}$$

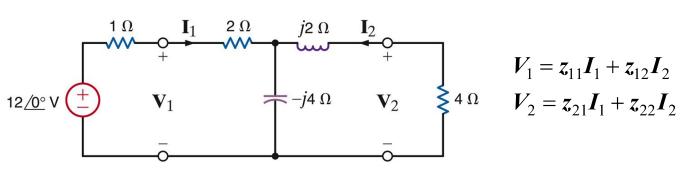
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$$V_1 = (2 - \mathbf{j}4)\mathbf{I}_1 - \mathbf{j}4\mathbf{I}_2$$
 $\Rightarrow \mathbf{z}_{11} = 2 - \mathbf{j}4\Omega$ $\mathbf{z}_{12} = -\mathbf{j}4\Omega$
 $V_2 = -\mathbf{j}4\mathbf{I}_1 - \mathbf{j}2\mathbf{I}_2$ $\mathbf{z}_{21} = -\mathbf{j}4\Omega$ $\mathbf{z}_{22} = -\mathbf{j}2\Omega$

LEARNING EXAMPLE

Use the Z parameters to find the current through the 4 Ohm resistor



Output port

constraint
$$V_2 = -4I_2$$

Input port

constraint
$$V_1 = 12 \angle 0^\circ - (1)I_1$$

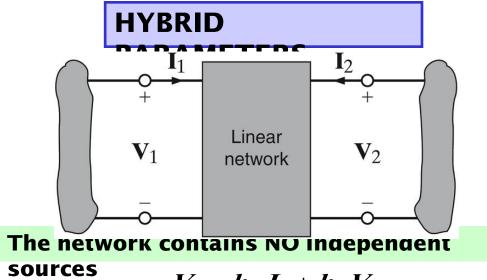
$$V_1 = (2 - j4)I_1 - j4I_2$$

$$V_2 = -j4I_1 - j2I_2$$

$$0 = -j4I_1 + (4 - j2)I_2 \times (3 - j4)$$

$$12 = (3 - j4)I_1 - j4I_2 \times j4$$

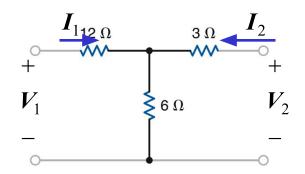
$$48j = (16 + (4 - j2)(3 - j4))I_2 \implies I_2 = 1.61 \angle 137.73^{\circ}$$



ources
$$oldsymbol{V}_1=oldsymbol{h}_{11}oldsymbol{I}_1+oldsymbol{h}_{12}oldsymbol{V}_2 \ oldsymbol{I}_2=oldsymbol{h}_{21}oldsymbol{I}_1+oldsymbol{h}_{22}oldsymbol{V}_2$$

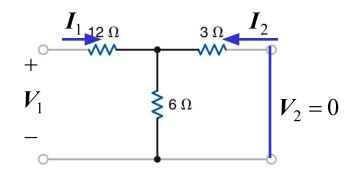
These parameters are very common in modeling transistors

Find the hybrid parameters for the network



$$V_1 = h_{11}I_1 + h_{12}V_2$$

 $I_2 = h_{21}I_1 + h_{22}V_2$



$$V_1 = (12 + (6 \parallel 3)) I_1 \Rightarrow h_{11} = 14\Omega$$

$$V_1 = \frac{6}{3+6}V_2 \Rightarrow h_{12} = \frac{2}{3}$$

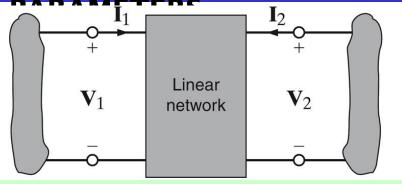
$$I_2 = -\frac{6}{3+6}I_1 \Longrightarrow h_{21} = -\frac{2}{3}$$

$$I_2 = \frac{V_2}{9} \Rightarrow h_{22} = \frac{1}{9} [S]$$

TRANSMISSION

ABCD

parameters



The network contains NO independent

sources

$$V_1 = AV_2 - BI_2$$

$$\boldsymbol{I}_1 = \boldsymbol{C}\boldsymbol{V}_2 - \boldsymbol{D}\boldsymbol{I}_2$$

$$A = \frac{V_1}{V_2} \bigg|_{I_2 = 0}$$

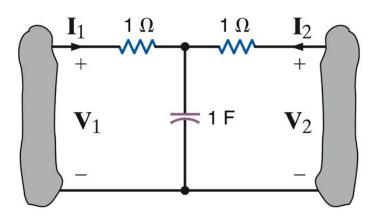
$$A = \frac{V_1}{V_2} \bigg|_{I_2 = 0} \qquad C = \frac{I_1}{V_2} \bigg|_{I_2 = 0}$$

A = open circuit voltage ratio

B = negative short-circuit transfer imperation $B = \frac{V_1}{I_2}\Big|_{V_2=0}$ $D = -\frac{I_1}{I_2}\Big|_{V_2=0}$ D = negative short-circuit transfer admittance D = negative short-circuit current ratioB = negative short - circuit transfer impedance

LEARNING EYAMPI E

Determine the transmission parameters



$$V_1 = AV_2 - BI_2$$

$$I_1 = CV_2 - DI_2$$

$$A = \frac{V_1}{V_2}\Big|_{I_2=0}$$

$$C = \frac{I_1}{V_2}\Big|_{I_2=0}$$

$$B = -\frac{V_1}{I_2}\Big|_{V_2=0}$$

$$D = -\frac{I_1}{I_2}\Big|_{V_2=0}$$

when
$$I_2 = 0$$

$$V_2 = \frac{\frac{1}{j\omega}}{1 + \frac{1}{j\omega}} V_1 \Rightarrow A = 1 + j\omega$$

$$V_2 = \frac{1}{j\omega} I_1 \Rightarrow \frac{I_1}{V_2} = j\omega$$

when
$$V_2 = 0$$

$$I_2 = -\frac{\frac{1}{j\omega}}{1 + \frac{1}{j\omega}}I_1 = -\frac{1}{1 + j\omega}I_1 \implies \mathbf{D} = 1 + j\omega$$

$$V_{1} = \left[1 + (1 \parallel \frac{1}{j\omega})\right] I_{1} = \left[\frac{2 + j\omega}{1 + j\omega}\right] \left[-(1 + j\omega)\right] I_{2}$$

$$B = 2 + j\omega$$

PARAMETER CONVERSIONS

If all parameters exist, they can be related by conventional algebraic manipulations.

As an example consider the relationship between Z and Y parameters

$$V_2 = z_{21}I_1 + z_{22}I_2$$

$$\begin{bmatrix} \boldsymbol{V}_1 \\ \boldsymbol{V}_2 \end{bmatrix} = \begin{bmatrix} \boldsymbol{z}_{11} & \boldsymbol{z}_{12} \\ \boldsymbol{z}_{21} & \boldsymbol{z}_{22} \end{bmatrix} \begin{bmatrix} \boldsymbol{I}_1 \\ \boldsymbol{I}_2 \end{bmatrix} \Rightarrow \begin{bmatrix} \boldsymbol{I}_1 \\ \boldsymbol{I}_2 \end{bmatrix} = \begin{bmatrix} \boldsymbol{z}_{11} & \boldsymbol{z}_{12} \\ \boldsymbol{z}_{21} & \boldsymbol{z}_{22} \end{bmatrix}^{-1} \begin{bmatrix} \boldsymbol{V}_1 \\ \boldsymbol{V}_2 \end{bmatrix} = \begin{bmatrix} \boldsymbol{y}_{11} & \boldsymbol{y}_{12} \\ \boldsymbol{y}_{21} & \boldsymbol{y}_{22} \end{bmatrix} \begin{bmatrix} \boldsymbol{V}_1 \\ \boldsymbol{V}_2 \end{bmatrix}$$

$$\begin{bmatrix} y_{11} & y_{12} \\ y_{21} & y_{22} \end{bmatrix} = \begin{bmatrix} z_{11} & z_{12} \\ z_{21} & z_{22} \end{bmatrix}^{-1} = \frac{1}{\Delta_{Z}} \begin{bmatrix} z_{22} & -z_{12} \\ -z_{21} & z_{11} \end{bmatrix}$$

with
$$\Delta_{Z} = z_{11}z_{22} - z_{21}z_{12}$$

In the following conversion table, the symbol Δ stands for the determinant of the corresponding matrix

$$\Delta_{\boldsymbol{Z}} = \begin{vmatrix} \boldsymbol{z}_{11} & \boldsymbol{z}_{12} \\ \boldsymbol{z}_{21} & \boldsymbol{z}_{22} \end{vmatrix}, \Delta_{\boldsymbol{Y}} = \begin{vmatrix} \boldsymbol{y}_{11} & \boldsymbol{y}_{12} \\ \boldsymbol{y}_{21} & \boldsymbol{y}_{22} \end{vmatrix}, \Delta_{\boldsymbol{H}} = \begin{vmatrix} \boldsymbol{h}_{11} & \boldsymbol{h}_{12} \\ \boldsymbol{h}_{21} & \boldsymbol{h}_{22} \end{vmatrix}, \Delta_{\boldsymbol{T}} = \begin{vmatrix} \boldsymbol{A} & \boldsymbol{B} \\ \boldsymbol{C} & \boldsymbol{D} \end{vmatrix}$$

TABLE 16.1 Two-port parameter conversion formulas

$$\begin{bmatrix} \mathbf{Z}_{11} & \mathbf{Z}_{12} \\ \mathbf{Z}_{21} & \mathbf{Z}_{22} \end{bmatrix}$$

$$\begin{bmatrix} \frac{\mathbf{z}_{22}}{\Delta_{\mathcal{Z}}} & \frac{-\mathbf{z}_{12}}{\Delta_{\mathcal{Z}}} \\ \frac{-\mathbf{z}_{21}}{\Delta_{\mathcal{Z}}} & \frac{\mathbf{z}_{11}}{\Delta_{\mathcal{Z}}} \end{bmatrix}$$

$$\begin{bmatrix} \mathbf{Z}_{11} & \Delta_{Z} \\ \mathbf{Z}_{21} & \mathbf{Z}_{21} \\ \end{bmatrix}$$

$$\begin{bmatrix} \mathbf{Z}_{11} & \Delta_{Z} \\ \mathbf{Z}_{21} & \mathbf{Z}_{22} \\ \mathbf{Z}_{21} & \mathbf{Z}_{21} \end{bmatrix}$$

$$\begin{bmatrix} \frac{\Delta_{Z}}{\mathbf{z}_{22}} & \frac{\mathbf{z}_{12}}{\mathbf{z}_{22}} \\ -\mathbf{z}_{21} & \frac{1}{\mathbf{z}_{22}} \end{bmatrix}$$

$$\begin{bmatrix} \frac{\mathbf{y}_{22}}{\Delta_{\gamma}} & \frac{-\mathbf{y}_{12}}{\Delta_{\gamma}} \\ \frac{-\mathbf{y}_{21}}{\Delta_{\gamma}} & \frac{\mathbf{y}_{11}}{\Delta_{\gamma}} \end{bmatrix} \qquad \begin{bmatrix} \frac{\mathbf{A}}{\mathbf{C}} & \frac{\Delta_{T}}{\mathbf{C}} \\ \frac{1}{\mathbf{C}} & \frac{\mathbf{D}}{\mathbf{C}} \end{bmatrix} \qquad \begin{bmatrix} \frac{\Delta_{H}}{\mathbf{h}_{22}} & \frac{\mathbf{h}_{12}}{\mathbf{h}_{22}} \\ \frac{-\mathbf{h}_{21}}{\mathbf{h}_{22}} & \frac{1}{\mathbf{h}_{22}} \end{bmatrix}$$

$$\begin{bmatrix} \mathbf{y}_{11} & \mathbf{y}_{12} \\ \mathbf{y}_{21} & \mathbf{y}_{22} \end{bmatrix}$$

$$\begin{bmatrix} \frac{\mathbf{z}_{11}}{\mathbf{z}_{21}} & \frac{\Delta_{Z}}{\mathbf{z}_{21}} \\ \frac{1}{\mathbf{z}_{21}} & \frac{\mathbf{z}_{22}}{\mathbf{z}_{21}} \end{bmatrix} \begin{bmatrix} \frac{-\mathbf{y}_{22}}{\mathbf{y}_{21}} & \frac{-1}{\mathbf{y}_{21}} \\ \frac{-\Delta_{Y}}{\mathbf{y}_{21}} & \frac{-\mathbf{y}_{11}}{\mathbf{y}_{21}} \end{bmatrix}$$

$$\begin{bmatrix} \frac{1}{\mathbf{y}_{11}} & \frac{-\mathbf{y}_{12}}{\mathbf{y}_{11}} \\ \frac{\mathbf{y}_{21}}{\mathbf{y}_{11}} & \frac{\Delta_{\gamma}}{\mathbf{y}_{11}} \end{bmatrix}$$

$$\begin{bmatrix} \mathbf{A} & \Delta_T \\ \mathbf{C} & \mathbf{C} \end{bmatrix}$$

$$\begin{bmatrix} \mathbf{1} & \mathbf{D} \\ \mathbf{C} & \mathbf{C} \end{bmatrix}$$

$$\begin{bmatrix} \frac{D}{B} & \frac{-\Delta_T}{B} \\ -\frac{1}{B} & \frac{A}{B} \end{bmatrix}$$

$$\begin{bmatrix} \frac{\mathbf{B}}{\mathbf{D}} & \frac{\Delta_T}{\mathbf{D}} \\ -\frac{\mathbf{1}}{\mathbf{D}} & \frac{\mathbf{C}}{\mathbf{D}} \end{bmatrix}$$

$$\begin{bmatrix} \frac{\Delta_{H}}{\mathbf{h}_{22}} & \frac{\mathbf{h}_{12}}{\mathbf{h}_{22}} \\ -\mathbf{h}_{21} & \frac{1}{\mathbf{h}_{22}} \end{bmatrix}$$

$$\begin{bmatrix} \frac{\mathbf{D}}{\mathbf{B}} & \frac{-\Delta_T}{\mathbf{B}} \\ -\frac{1}{\mathbf{B}} & \frac{\mathbf{A}}{\mathbf{B}} \end{bmatrix} \begin{bmatrix} \frac{1}{\mathbf{h}_{11}} & \frac{-\mathbf{h}_{12}}{\mathbf{h}_{11}} \\ \frac{\mathbf{h}_{21}}{\mathbf{h}_{11}} & \frac{\Delta_H}{\mathbf{h}_{11}} \end{bmatrix}$$

$$\begin{bmatrix} \frac{-\Delta_H}{\mathbf{h}_{21}} & \frac{-\mathbf{h}_{11}}{\mathbf{h}_{21}} \\ \frac{-\mathbf{h}_{22}}{\mathbf{h}_{21}} & \frac{-1}{\mathbf{h}_{21}} \end{bmatrix}$$

$$\begin{bmatrix} \mathbf{h}_{11} & \mathbf{h}_{12} \\ \mathbf{h}_{21} & \mathbf{h}_{22} \end{bmatrix}$$

INTERCONNECTION OF

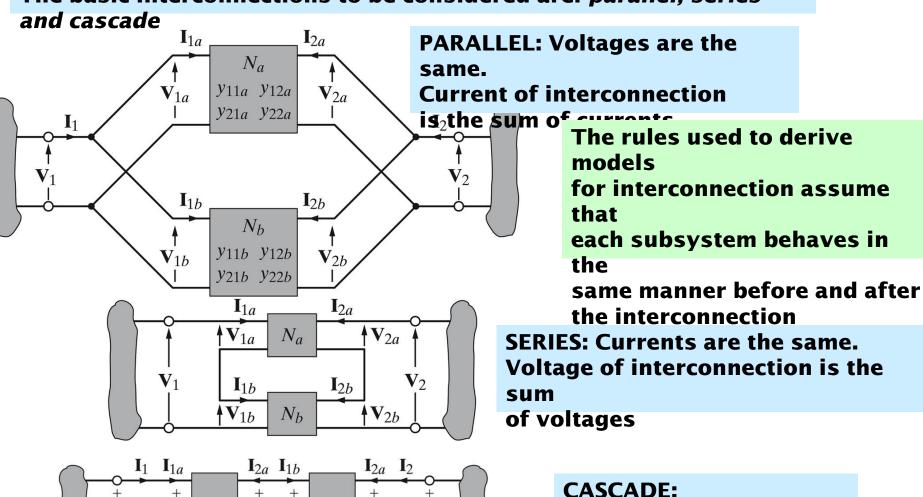
Interconnections permit the description of complex systems in terms of simpler

The basic interconnections to be considered are: parallel, series

 N_a

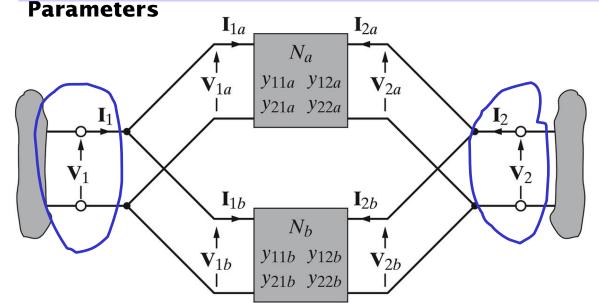
 N_b

 \mathbf{V}_{2b}



Output of first subsystem acts as input for the

Parallel Interconnection: Description Using Y



Interconnection description

$$\begin{bmatrix} \mathbf{I}_1 \\ \mathbf{I}_2 \end{bmatrix} = \begin{bmatrix} \mathbf{y}_{11} & \mathbf{y}_{12} \\ \mathbf{y}_{21} & \mathbf{y}_{22} \end{bmatrix} \begin{bmatrix} \mathbf{V}_1 \\ \mathbf{V}_2 \end{bmatrix}$$
$$\mathbf{I} = \mathbf{Y}\mathbf{V}$$

$$I_a = \begin{bmatrix} I_{1a} \\ I_{2a} \end{bmatrix}, V_a = \begin{bmatrix} V_{1a} \\ V_{2a} \end{bmatrix}, Y_a = \begin{bmatrix} y_{11a} & y_{12a} \\ y_{21a} & y_{22b} \end{bmatrix} \Rightarrow I_a = Y_a V_a$$
 In a similar manner $I_b = Y_b V_b$

$$I_b = Y_b V_b$$

Interconne ction constraint s:

$$I_{1} = I_{1a} + I_{1b}, \ I_{2} = I_{2a} + I_{2b}$$

$$V_{1} = V_{1a} = V_{1b}, \ V_{2} = V_{2a} = V_{2b}$$

$$\Rightarrow \begin{cases} I = I_{a} + I_{b} \\ V = V_{a} = V_{b} \end{cases} \Rightarrow I = Y_{a}V_{a} + Y_{b}V_{b} = (Y_{a} + Y_{b})V$$

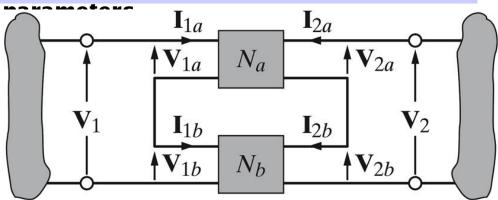
$$Y = Y_{a} + Y_{b}$$

$$\Rightarrow \begin{cases} I = I_a + I_b \\ V = V_a = V_b \end{cases}$$

$$\Rightarrow I = Y_a V_a + Y_b V_b = (Y_a + Y_b) V_b$$

$$Y = Y_a + Y_b$$

Series interconnection using Z



 $\Rightarrow V = Z_a I + Z_b I = (Z_a + Z_b) I$

Interconnection constraints

$$I_a = I_b = I$$
$$V = V_a + V_b$$

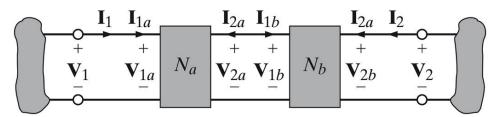
SERIES: Currents are the same. Voltage of interconnection is the sum

of voltages Description of each subsystem

$$V_a = Z_a I_a, \quad V_b = Z_b I_b$$

$$Z = Z_a + Z_b$$

Cascade connection using transmission parameters



Interconnection constraints:

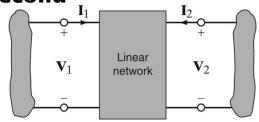
$$I_{2a} = -I_{1b}$$
 $V_{2a} = V_{1b}$
 $V_{1} = V_{1a}$ $V_{2} = V_{2b}$
 $I_{1} = I_{1a}$ $I_{2} = I_{2b}$

$$\begin{bmatrix} V_{1a} \\ I_{1a} \end{bmatrix} = \begin{bmatrix} A_a & B_a \\ C_a & D_a \end{bmatrix} \begin{bmatrix} V_{2a} \\ -I_{2a} \end{bmatrix}$$

$$\begin{bmatrix} V_{1b} \\ I_{1b} \end{bmatrix} = \begin{bmatrix} A_b & B_b \\ C_b & D_b \end{bmatrix} \begin{bmatrix} V_{2b} \\ -I_{2b} \end{bmatrix}$$
$$\begin{bmatrix} V_1 \\ A_a \end{bmatrix}$$

Output of first subsystem acts as input for the second

CASCADE:



$$V_1 = AV_2 - BI_2$$
$$I_1 = CV_2 - DI_2$$

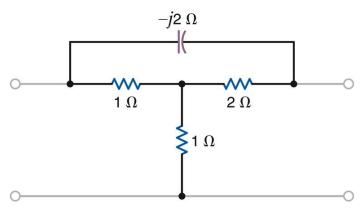
$$\begin{bmatrix} \boldsymbol{V}_1 \\ \boldsymbol{I}_1 \end{bmatrix} = \begin{bmatrix} \boldsymbol{A} & \boldsymbol{B} \\ \boldsymbol{C} & \boldsymbol{D} \end{bmatrix} \begin{bmatrix} \boldsymbol{V}_2 \\ -\boldsymbol{I}_2 \end{bmatrix}$$

Matrix multiplication does not commute.

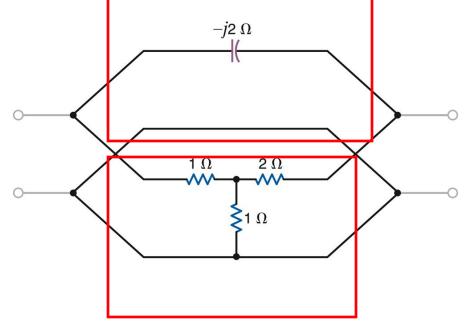
Order of the interconnection is important $\mathbf{R} \supset \mathbf{L} \supset \mathbf{L}$

$$\begin{bmatrix}
V_1 \\
I_1
\end{bmatrix} = \begin{bmatrix}
A_a & B_a \\
C_a & D_a
\end{bmatrix} \begin{bmatrix}
A_b & B_b \\
C_b & D_b
\end{bmatrix} \begin{bmatrix}
V_2 \\
-I_2
\end{bmatrix}$$

Find the Y parameters for the



network

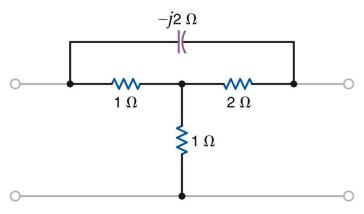


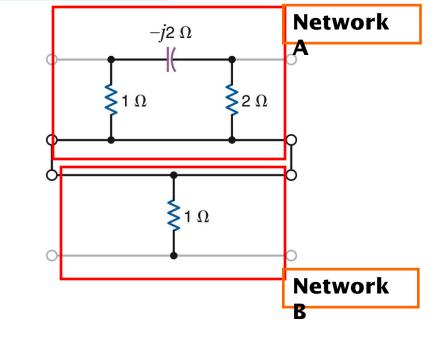
$$y_{11a} = j\frac{1}{2}, \ y_{12a} = -j\frac{1}{2}$$

$$I_1$$
 I_2
 I_2
 I_1
 I_2
 I_2

Find the Z parameters of the

EXAMPLE network





Use direct method, or given the Y parameters transform to Z

... or decompose the network in a

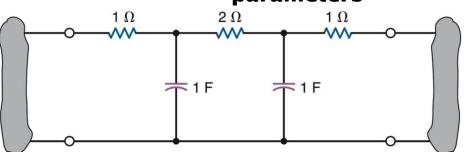
seriesconnection of simpler networks

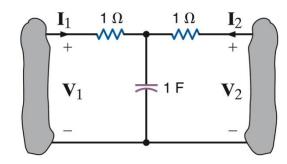
$$\boldsymbol{Z}_{a} = \begin{vmatrix} 3-2\boldsymbol{j} & 3-2\boldsymbol{j} \\ \frac{2}{3-2\boldsymbol{j}} & \frac{2-4\boldsymbol{j}}{3-2\boldsymbol{j}} \end{vmatrix}$$

$$\boldsymbol{Z_b} = \begin{bmatrix} 1 & 1 \\ 1 & 1 \end{bmatrix}$$

$$Z = Z_a + Z_b = \begin{bmatrix} \frac{5-4j}{3-2j} & \frac{5-2j}{3-2j} \\ \frac{5-2j}{3-2j} & \frac{5-6j}{3-2j} \end{bmatrix}$$

Find the transmission parameters





By splitting the 2-Ohm resistor, the network can be viewed as the cascade connection of two identical

$$\begin{bmatrix} A & B \\ C & D \end{bmatrix} = \begin{bmatrix} 1 + j\omega & 2 + j\omega \\ j\omega & 1 + j\omega \end{bmatrix}$$

$$\begin{bmatrix} \mathbf{A} & \mathbf{B} \\ \mathbf{A} & \mathbf{B} \end{bmatrix} = \begin{bmatrix} 1 + \boldsymbol{j}\omega & 2 + \boldsymbol{j}\omega \\ \boldsymbol{j}\omega & 1 + \boldsymbol{j}\omega \end{bmatrix} \begin{bmatrix} 1 + \boldsymbol{j}\omega & 2 + \boldsymbol{j}\omega \\ \boldsymbol{j}\omega & 1 + \boldsymbol{j}\omega \end{bmatrix}$$

$$\begin{bmatrix} \boldsymbol{A} & \boldsymbol{B} \\ \boldsymbol{C} & \boldsymbol{D} \end{bmatrix} = \begin{bmatrix} (1+\boldsymbol{j}\omega)^2 + (2+\boldsymbol{j}\omega)\boldsymbol{j}\omega & (1+\boldsymbol{j}\omega)(2+\boldsymbol{j}\omega) + (2+\boldsymbol{j}\omega)(1+\boldsymbol{j}\omega) \\ \boldsymbol{j}\omega(1+\boldsymbol{j}\omega) + (1+\boldsymbol{j}\omega)(\boldsymbol{j}\omega) & \boldsymbol{j}\omega(2+\boldsymbol{j}\omega) + (1+\boldsymbol{j}\omega)^2 \end{bmatrix}$$

$$\begin{bmatrix} \mathbf{A} & \mathbf{B} \\ \mathbf{C} & \mathbf{D} \end{bmatrix} = \begin{bmatrix} 1 + 4\mathbf{j}\omega - 2\omega^2 & 4 + 6\mathbf{j}\omega - 2\omega^2 \\ 2\mathbf{j}\omega - 2\omega^2 & 1 + 4\mathbf{j}\omega - 2\omega^2 \end{bmatrix}$$