

# Технологии походов

Как наука помогает делать экипировку лучше?

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10-1

$w = 2\pi f = 2\pi/T$   
 $F_d = -bv$   
 $x(t) = x_m e^{-\frac{b}{2m}t} \cos(\omega t + \phi)$   
 $\omega = \sqrt{\frac{k}{m} - \frac{b^2}{4m^2}}$   
 $E(t) = \frac{1}{2} k x_m^2 e^{-\frac{b}{m}t}$   
 $E_{tot} = U + K$   
 $v(t) = \frac{1}{2} k x^2$   
 $k(t) = \frac{1}{2} m v^2$   
 $\text{critical damp } b^2 = 4km$   
 $\text{under damped } b^2 < 4km$   
 $\text{over damped } b^2 > 4km$   
 $PE = mgh$   
 $T = 2\pi \sqrt{\frac{L}{g}}$  simple pend  
 $T = 2\pi \sqrt{\frac{I}{mgh}}$  physical pend  
 $v(t) = -\omega x_m \sin(\omega t + \phi)$   
 $x(t) = x_m \cos(\omega t + \phi)$   
 $a(t) = -\omega^2 x(t)$   
 $Y(x,t) = y_m \sin(kx - \omega t)$   
 $k = \frac{2\pi}{\lambda}$   
 $v = \frac{\omega}{k} = \frac{\lambda}{T} = \lambda f$   
 $v = \sqrt{\frac{T}{\mu}}$   
 $v = \frac{\text{mass}}{\text{length}}$   
 $P_{ave} = \frac{1}{2} v v_m^2$

resonance  $\lambda = \frac{2L}{n}$   $n=1,2,3$   
 $f = \frac{v}{\lambda} = \frac{n v}{2L}$   $n=1,2,3$   
 $v = \sqrt{\frac{B}{\rho}}$  Bulk modulus  
 $\Delta P_n = v \rho \omega S_m$  displacement  
 $f_{beat} = |f_1 - f_2|$   
 $I = \frac{\text{Power}}{\text{Area}} = \frac{P_s}{4\pi r^2}$   
 $P_m = 2PVI$   
 $P_m = v \rho \omega S_m$   
 $I = \frac{1}{2} \rho v \omega^2 S_m^2$   
 $\sin \theta = \frac{v_2}{v_1}$   
 $v_2/v_1 = \text{mach \#}$   
 $\Delta L = 0.5, 1.5, 2.5$  fully destructive  
 $\Delta L = L \alpha \Delta T$   
 $T_F = \frac{9}{5} T_C + 32$   
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 $\Delta L = L \alpha \Delta T$   
 $\Delta V = V \beta \Delta T$   
 $Q = C \Delta T$  Heat capacity  
 $Q = C_m \Delta T$  specific heat  
 $Q = L_m$  Heat of transformation  
 $Q = \int v p dv$

$R = \frac{L}{k}$   
 $P_{cond} = \frac{Q}{t} = k \frac{T_h - T_c}{L}$   
 $P_{rad} = \sigma \epsilon A T^4$   
 $P_{net} = P_{abs} - P_{rad}$   
 $P_{abs} = \sigma \epsilon A T_{env}^4$   
 $Q = n C_p \Delta T$  (constant pressure)  
 $Q = n C_v \Delta T$  (constant volume)  
 $W = P \Delta V = n R \Delta T$  (constant pressure)  
 $T_1 V_1^{\gamma-1} = T_2 V_2^{\gamma-1}$   
 $P_1 V_1^\gamma = P_2 V_2^\gamma$  (adiabatic)  
 $\Delta S = \int \frac{dQ}{T}$   
 $\Delta S = \frac{Q}{T_{ave}}$  Small  $\Delta T$   
 $\Delta S = n R \ln \left( \frac{V_2}{V_1} \right) + n C_v \ln \left( \frac{T_2}{T_1} \right)$

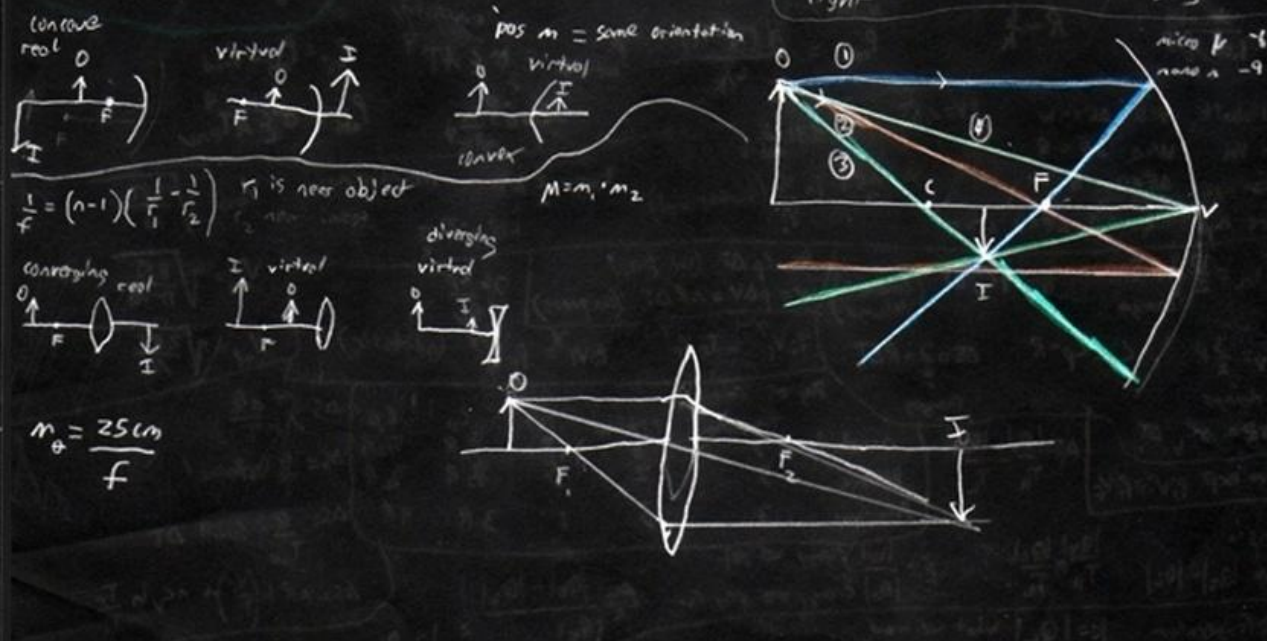
$n = \frac{\text{molecules}}{6.02 \times 10^{23}}$   
 $R = \frac{L}{k}$   
 $P_{cond} = \frac{A(T_h - T_c)}{\sum L/k}$   
 $P_{rad} = \sigma \epsilon A T^4$   
 $P_{net} = P_{abs} - P_{rad}$   
 $P_{abs} = \sigma \epsilon A T_{env}^4$   
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$\Delta E = n C_v \Delta T$   
 $\Delta S = \frac{Q_h}{T_h} - \frac{Q_c}{T_c}$   
 $\Delta S = \frac{Q}{T_{ave}}$  Small  $\Delta T$   
 $\Delta S = n R \ln \left( \frac{V_2}{V_1} \right) + n C_v \ln \left( \frac{T_2}{T_1} \right)$   
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Polarization  $I = I_0 \cos^2 \theta$   
 refraction  $n_1 \sin \theta_1 = n_2 \sin \theta_2$   
 critical angle  $\theta_c = \sin^{-1} \frac{n_2}{n_1}$   
 Brewster's angle  $\theta_B = \tan^{-1} \frac{n_2}{n_1}$   
 Thin film  $2L = (m + \frac{1}{2}) \frac{\lambda}{n_2}$  maxima  
 $2L = \frac{m \lambda}{n_2}$  minima  
 $\Delta L = d \sin \theta$   
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Single slit diffraction  $a \sin \theta = m \lambda$   $(m=1,2,3)$  minima  
 $I = I_m \left( \frac{\sin A}{A} \right)^2$   
 $A = \frac{1}{2} \theta = \frac{\pi a}{\lambda} \sin \theta$   
 Diffraction grating  $d \sin \theta = m \lambda$   $(m=0,1,2)$  maxima lines  
 Circular Diffraction  $\theta = 1.22 \frac{\lambda}{d}$  Rayleigh criterion  
 $\sin \theta = 1.22 \frac{\lambda}{d}$  first minimum  
 Plane mirrors  $i = -p$   
 $\theta = 1.22 \frac{\lambda}{d}$  Rayleigh criterion  
 $\sin \theta = 1.22 \frac{\lambda}{d}$  first minimum  
 $\Delta \theta \approx \frac{\lambda}{Nd \cos \theta}$  half width  
 $R = Nm$  resolving power  
 $D = \frac{m}{d \cos \theta}$  dispersion  
 $f = \frac{\text{radius of curvature}}{2}$   
 $\frac{1}{p} + \frac{1}{i} = \frac{1}{f}$  spherical mirror  
 $|m| = \frac{h'}{h}$   
 $m = -\frac{i}{p}$

concave real  $0$   
 virtual  $0$   
 convex  $0$   
 concave real  $0$   
 virtual  $0$   
 convex  $0$   
 concave real  $0$   
 virtual  $0$   
 convex  $0$   
 $\frac{1}{f} = (n-1) \left( \frac{1}{r_1} - \frac{1}{r_2} \right)$   
 $M = m_1 m_2$   
 $m = \frac{25 \text{ cm}}{f}$



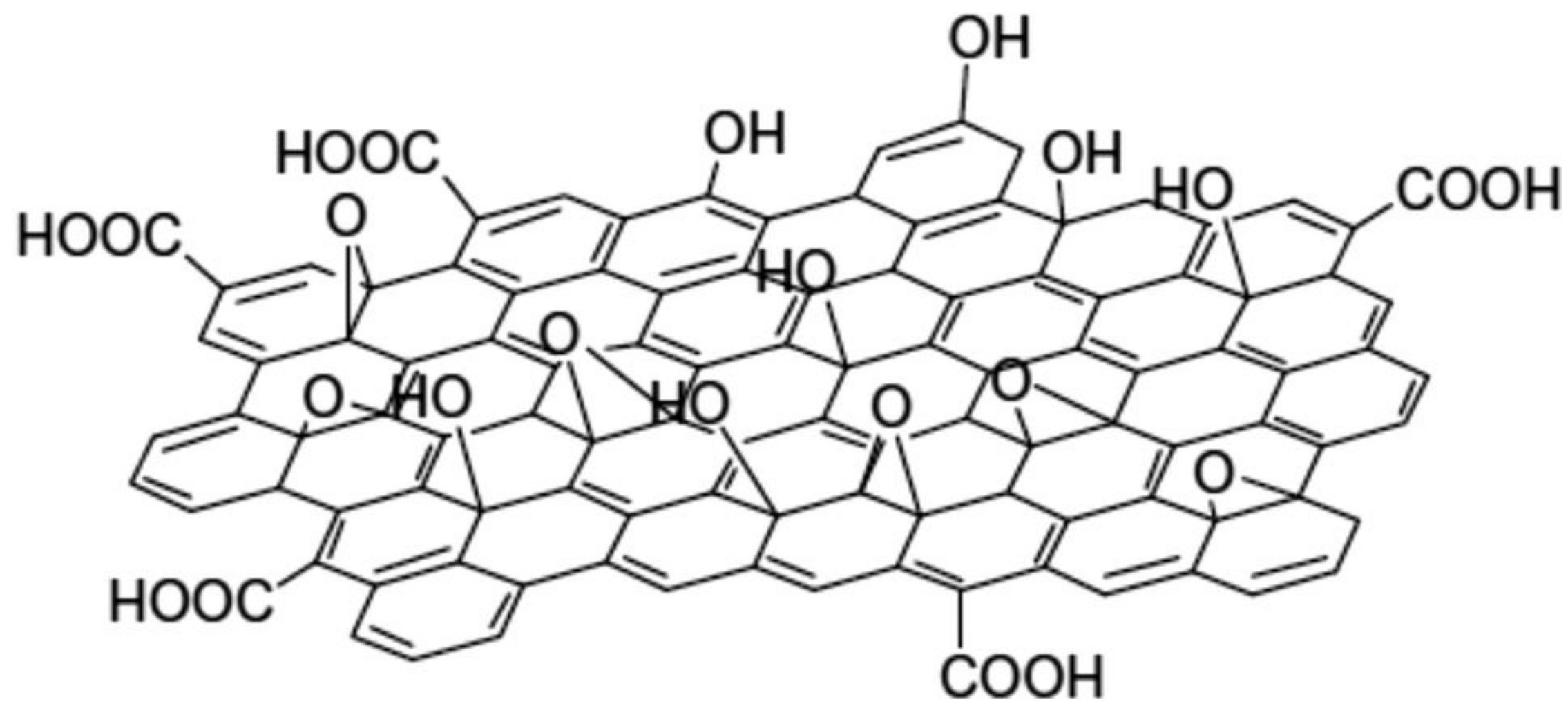


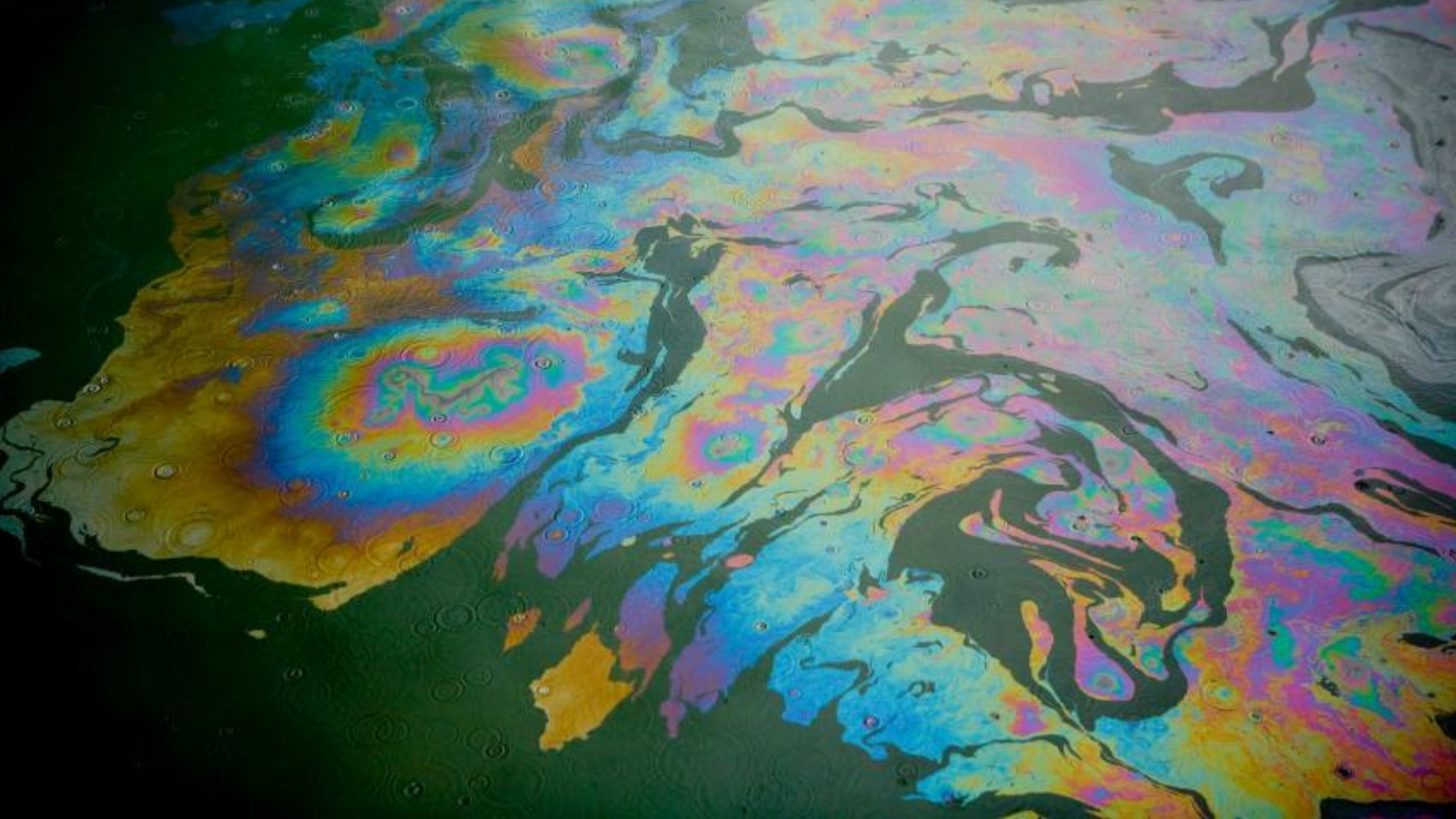




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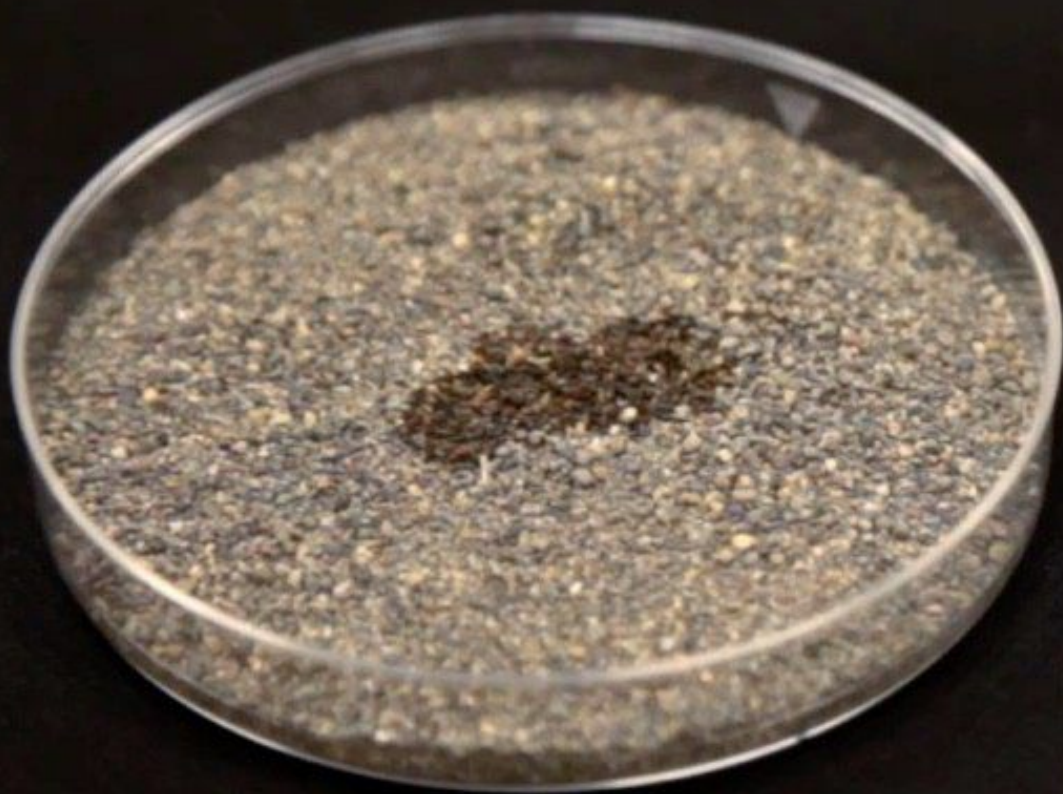


MOUNTAIN  
HARD  
WEAR

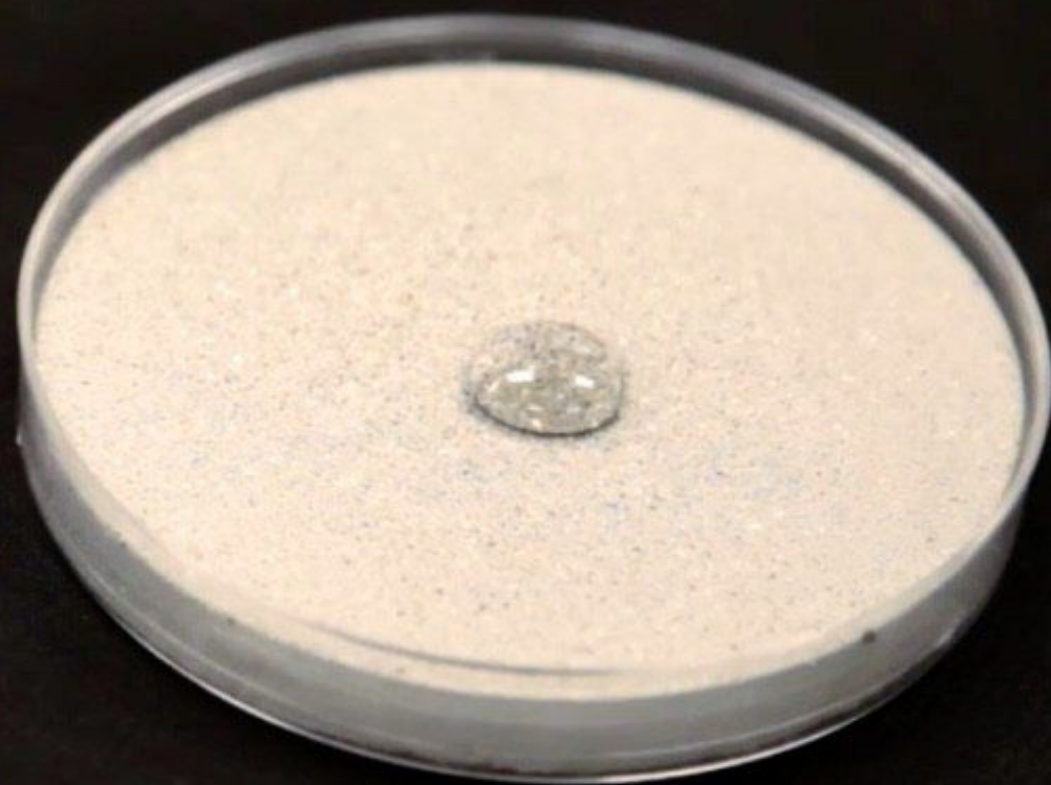




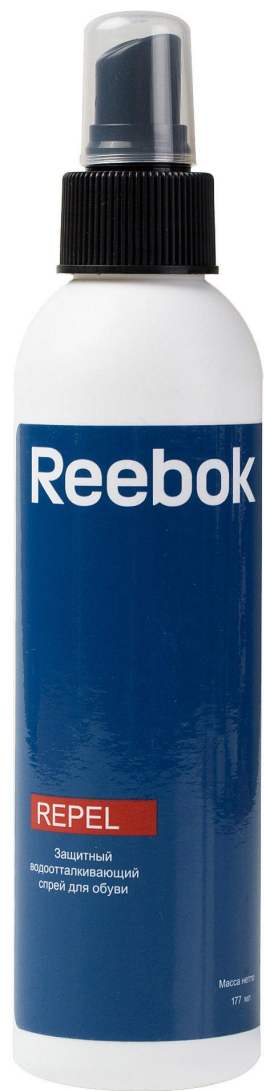




**SAND**



**CONCRETE**







HIGH PEAK

RAPIDO 3









**Спасибо за  
внимание**

